

Investigation of Local Flow Phenomena of Misaligned Riblets in a Turbulent Boundary Layer

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**Investigation of
Local Flow
Phenomena of
Misaligned Riblets
in a Turbulent
Boundary Layer**

Motivation

Method/Validation

Results

Conclusions

Outline

- 1. Motivation**
- 2. Method and Validation**
- 3. Results**
- 4. Conclusions**



Riblets in Industrial Applications (e.g. Gas Turbine Engines)

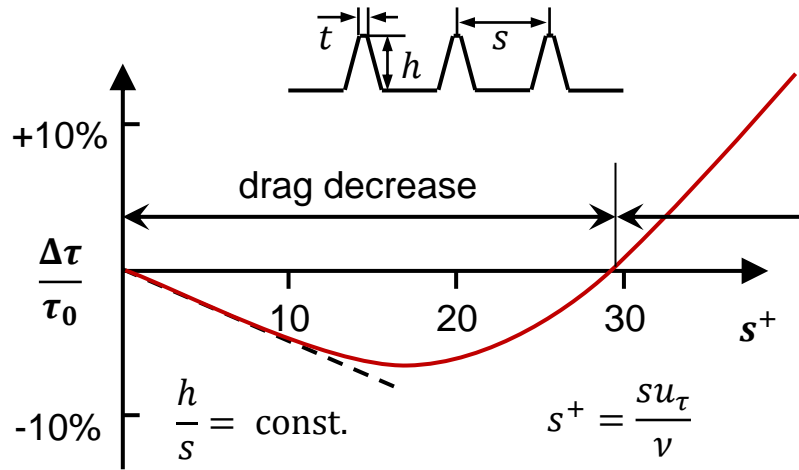
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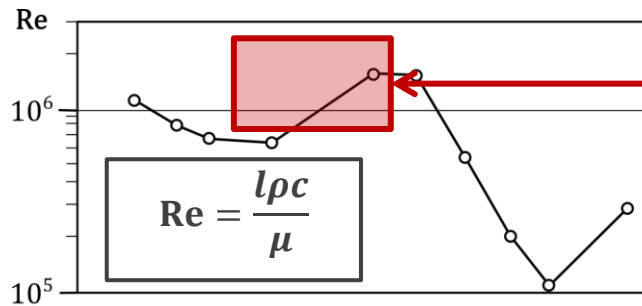
Results

Conclusions



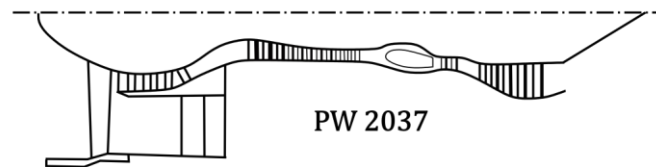
Prospects

- In turbulent boundary layers
- Up to **10% drag reduction** for ideal riblets
- Changing potential for varying geometry/operating point
- **Severe Drag increase possible**



High- and intermediate pressure compressor

- High Re
- Subsonic flow
- Erosion less severe
- Stationary gas turbines even more appropriate



Reynolds number at cruise of typical mid-thrust mid-range engine



Estimation of Riblet Potential for a 4.5 Stage Compressor

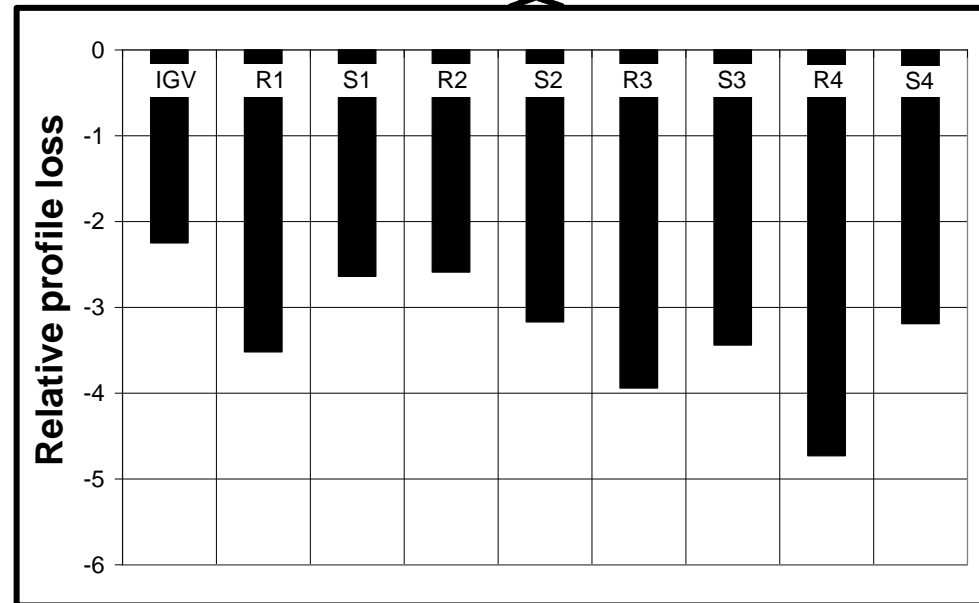
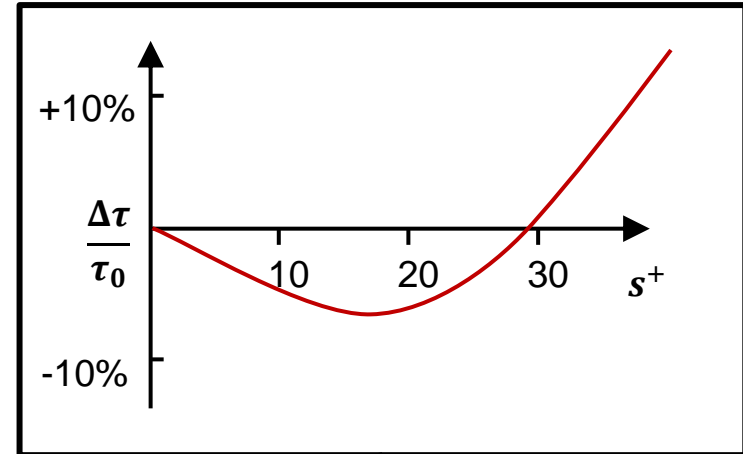
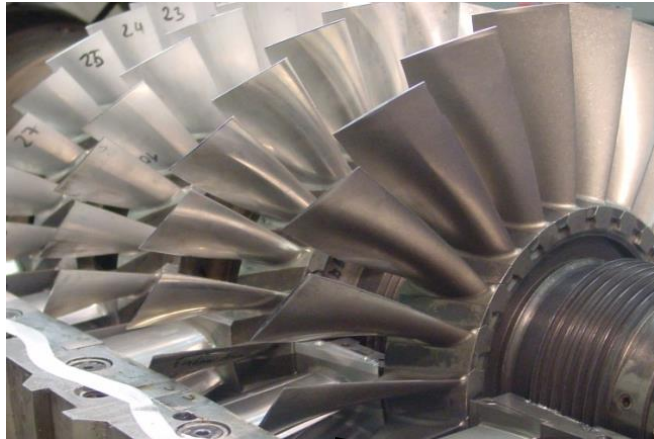
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Relative increase of adiabatic efficiency at design point: approx. 0.2%



Aerodynamic Challenges for the Application in Turbomachinery

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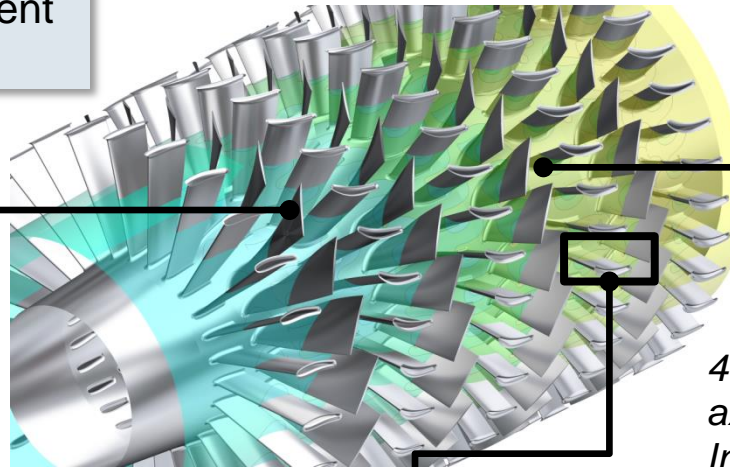
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Pressure gradient effects

Change in blade loading



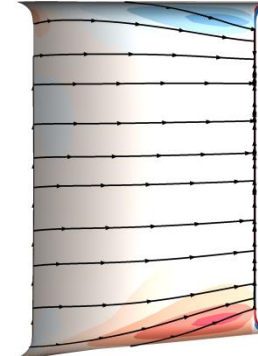
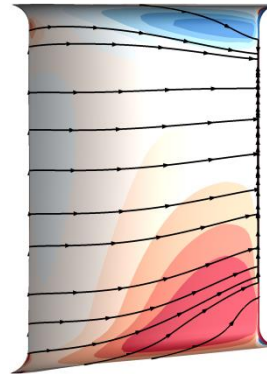
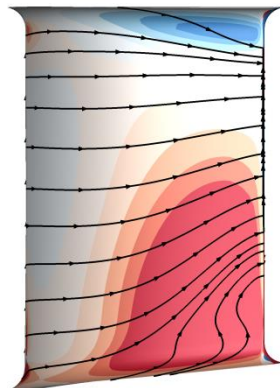
4.5 stage high-speed axial compressor
Institute of Turbomachinery and Fluid Dynamics

Variation of flow directions with operating point

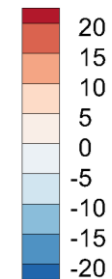
Near Stall

Best Efficiency

Near Choke



Pitch Angle in Degree

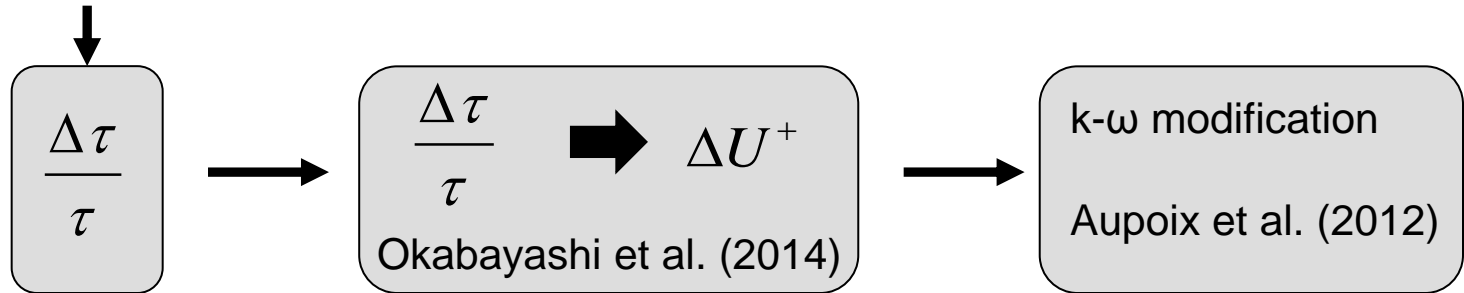


Suction side streamlines stator 3



Proposed RANS-Model¹

Ideal and manufactured Riblets



$$\frac{D\omega}{Dt} = 2\gamma s_{ij}s_{ij} - f_{damp} \cdot \beta\omega^2 + \frac{\partial}{\partial x_j} \left[(\nu + \sigma_\omega \nu_t) \frac{\partial \omega}{\partial x_j} \right]$$

$$f_{damp} = 1 - A \exp\left(-\frac{\omega y^2}{500\nu}\right)$$

Effect of Misalignment

Adapted Pressure Gradient Effect calculation

Improved drag increase regime prediction

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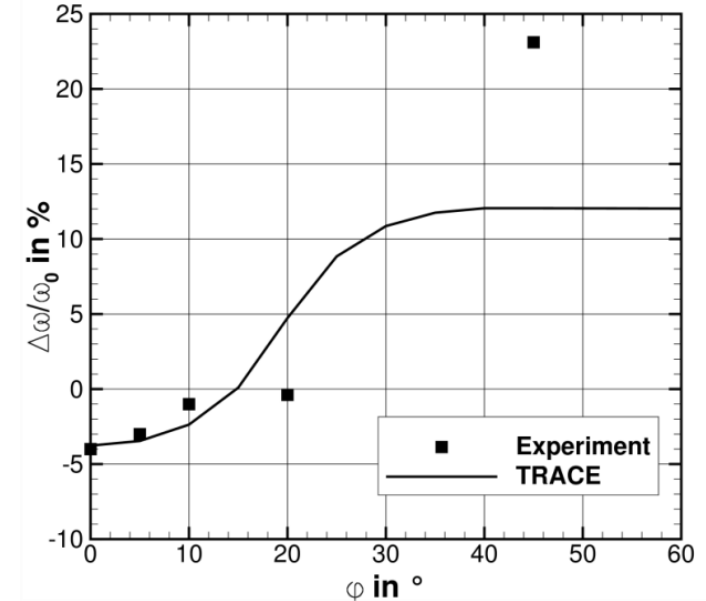
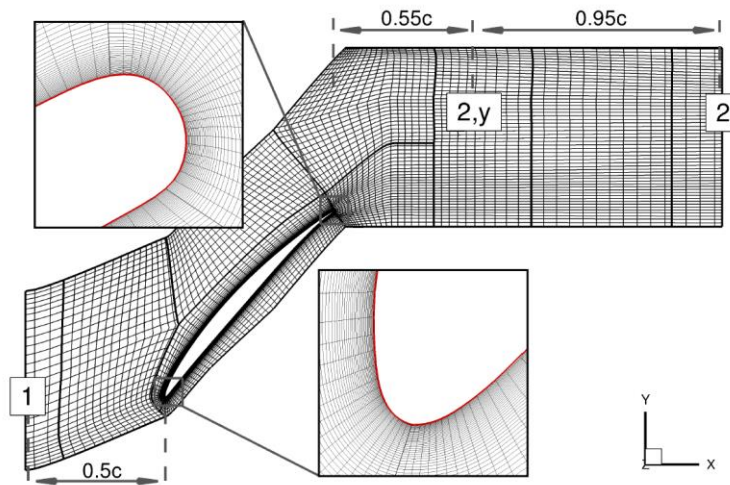
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¹Koepplin V., Herbst F.; Seume JR. (2017): Correlation-Based Riblet Model for Turbomachinery Applications. ASME Journal of Turbomachinery;139(7)



RANS-Predictions¹ of Integral Effect: Compressor Cascade



Relative change of total pressure (profile) loss

$$\omega_{\text{loss}} = \frac{p_{\text{tot,in}} - p_{\text{tot,out}}}{p_{\text{tot,in}} - p_{\text{in}}}$$

- predicted excellent for aligned Riblets
- deviates for misaligned Riblets
- alternating under- and over-prediction with increasing misalignment

¹Koepplin V., Herbst F.; Seume JR. (2017): Correlation-Based Riblet Model for Turbomachinery Applications. ASME Journal of Turbomachinery;139(7)



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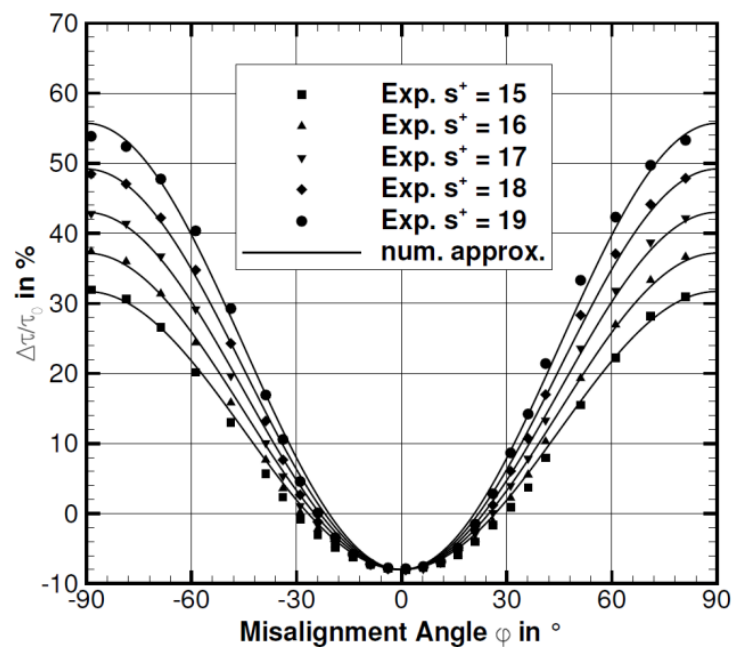
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Objectives of this Misalignment Study



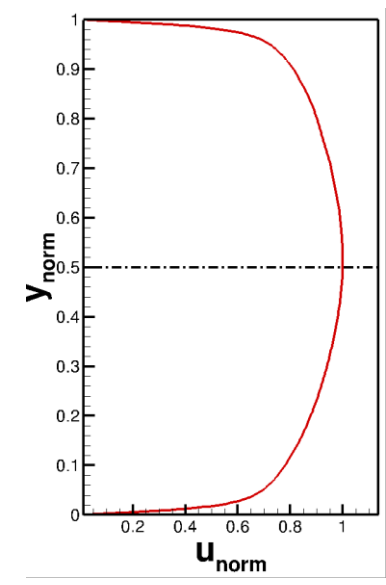
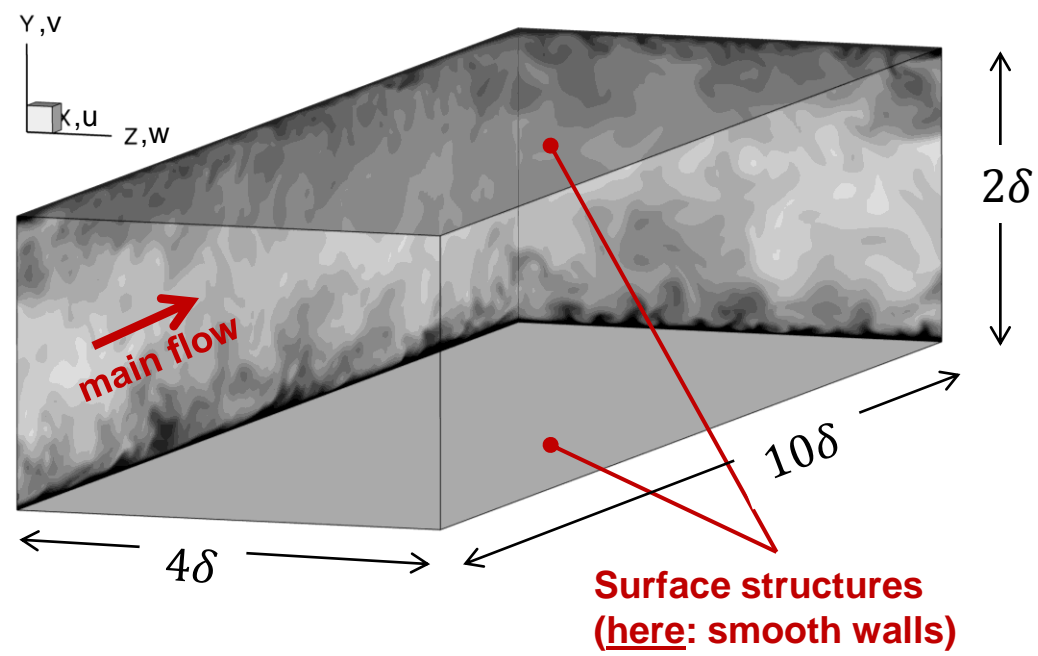
- Increase quantitative data base for correlation-based RANS-model
- Understand locally relevant flow features to criticize chosen RANS-modeling strategy
- Setup reliable DNS for prediction of Riblet misalignment in turbulent boundary layers



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Numerical Method and Principal Setup



Setup und Boundary Conditions

- Plane channel flow
- Periodic in stream- and spanwise direction
- No-slip walls at bottom and top
- $Re_\tau = 395$ with $Re_B = 14000$
- Spatial resolution:
 - $\Delta y^+ = 0.4 \dots 10$
 - $\Delta x^+ = 10$
 - $\Delta z^+ = 5$

Flow Solver

- OpenFoam
- Finite Volume
- Spatial discretization: bounded 2nd order TVD scheme
- Time integration: 2nd order Euler backward (implicit)

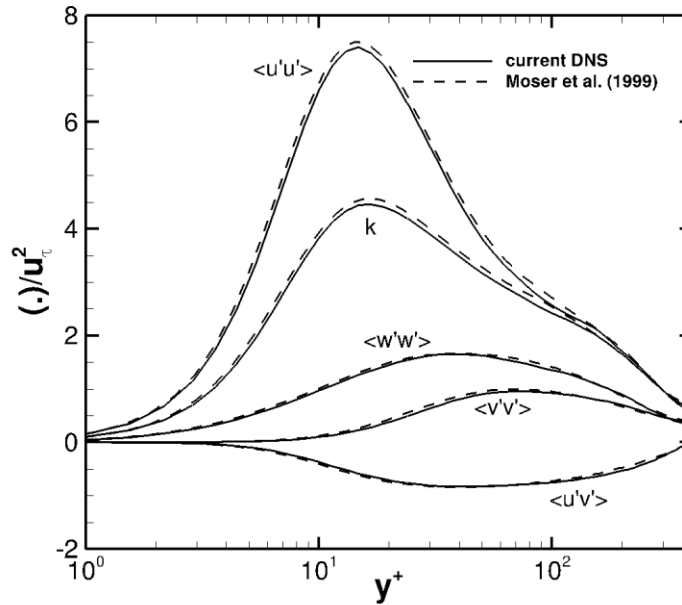


Validation for Smooth Wall at $Re_\tau = 395$

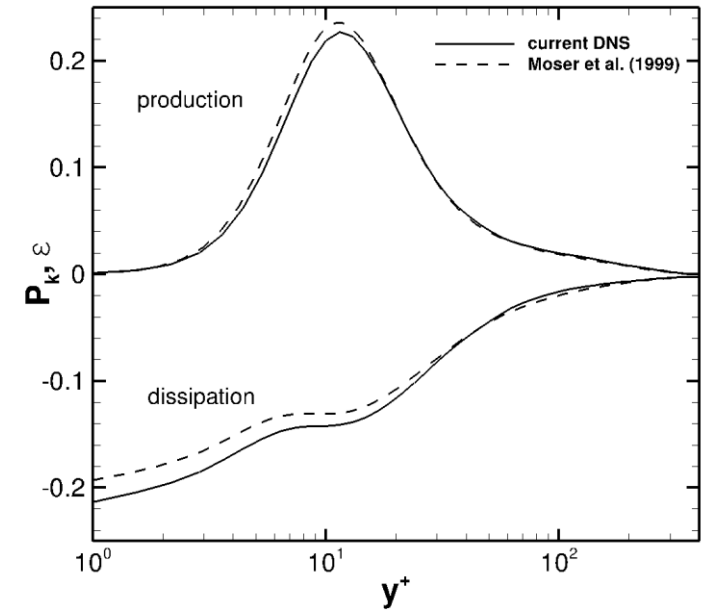
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Reynolds Stresses



Turbulent Kinetic Energy Balance



All quantities averaged over $t^+ \approx 120$

Reynolds stresses and turbulence kinetic energy balance in (very) good accordance with Moser et al. (1999)



Aligned Riblets: Numerical Setup

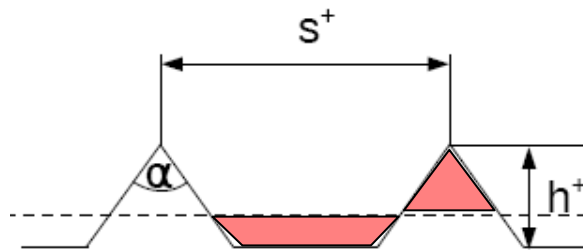
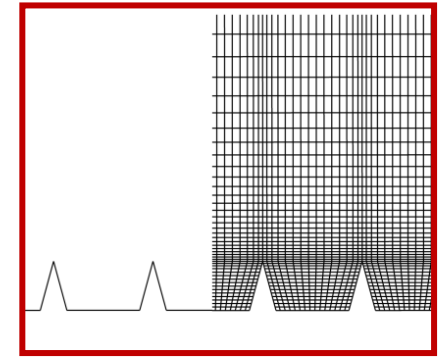
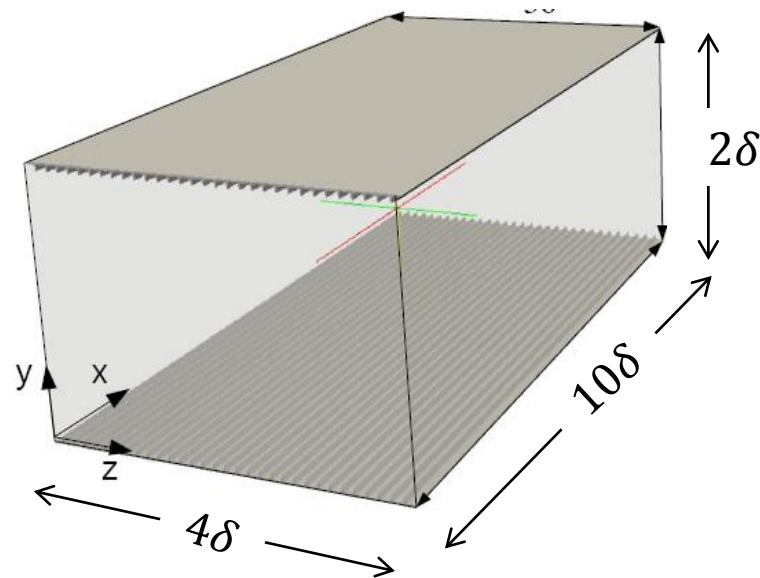
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Setup und Boundary Conditions

- Ideal trapezoidal Riblets
- Variation of Riblet spacing s^+
- Riblet height $h^+ = 0.5s^+$
- Riblet tip-angle: $\alpha = 30^\circ$
- Body-fitted hexa mesh
- $Re_\tau = 395$ with $Re_B = 14000$
- $Re_\tau = 180$ with $Re_B = 5700$

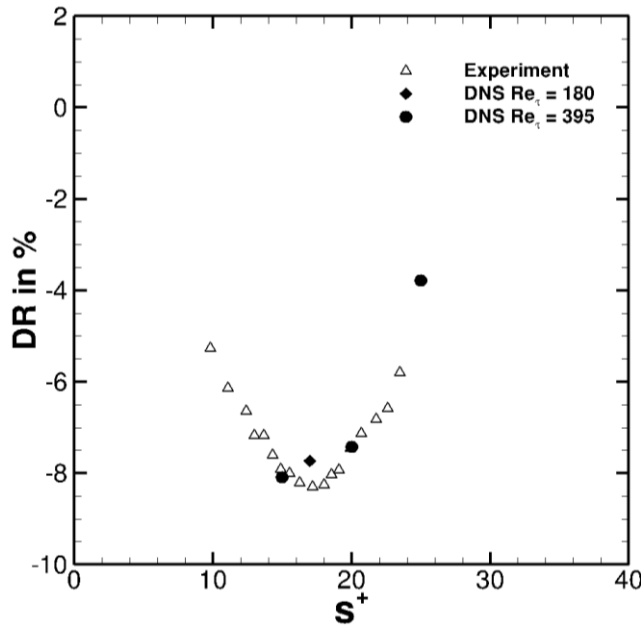


Predicted Drag Reduction of Aligned Riblets

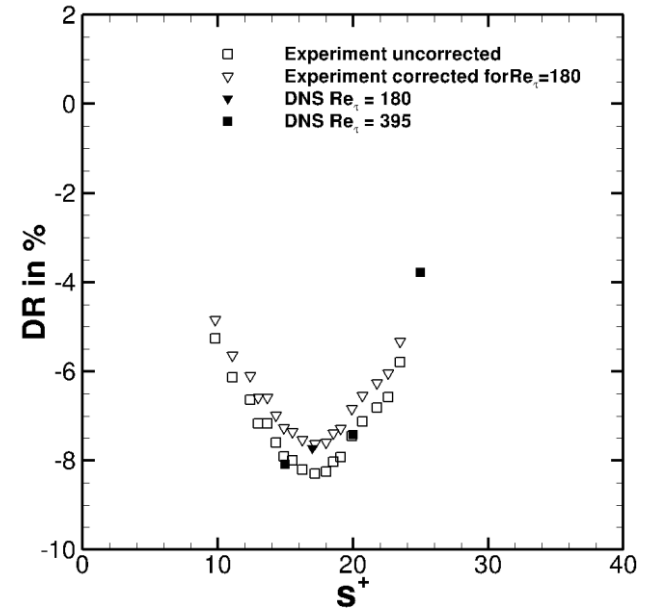
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Experimental Data¹



Adjusted Exp. Data



- Excellent prediction of experimental drag reduction (DR) for $Re_\tau = 395$ and
- for adjusted experimental data of $Re_\tau = 180$
- Experiments adjusted for Reynolds number according to²

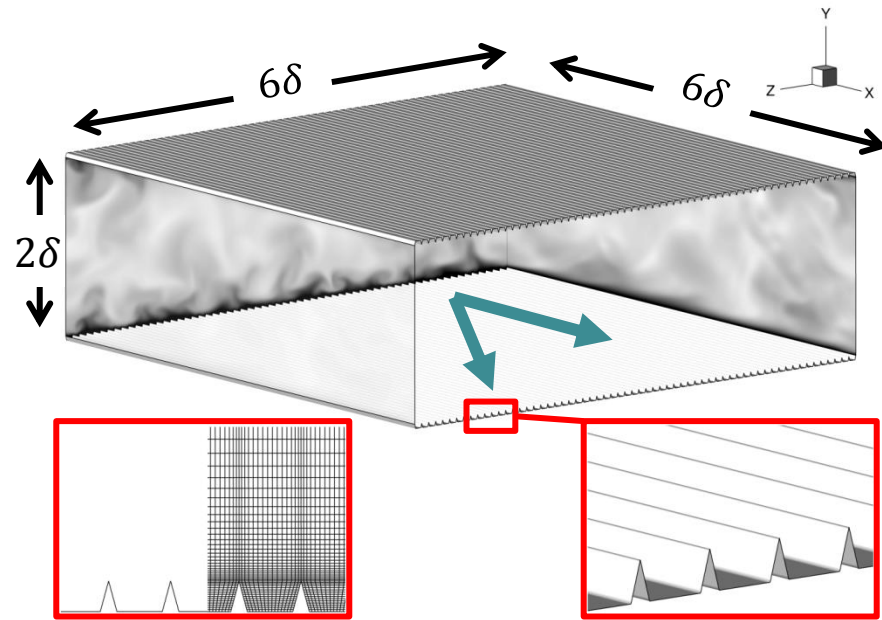
$$\Delta U^+ = - \left[(2C_{f0})^{-\frac{1}{2}} + (2\kappa)^{-1} \right] \frac{\Delta C_f}{C_{f0}}$$

¹Exp. data acc. to: Hage, W. (2004): Zur Widerstandsverminderung von dreidimensionalen Riblet-Strukturen und anderen Oberflächen. PhD Thesis, TU Berlin

²Garcia-Mayoral, R.; Jimenez, J. (2011): Drag Reduction by Riblets. Philos. Trans. R. Soc. A, 369(1940), pp. 1412–1427.



Misaligned Riblets: Numerical Setup



Setup und Boundary Conditions

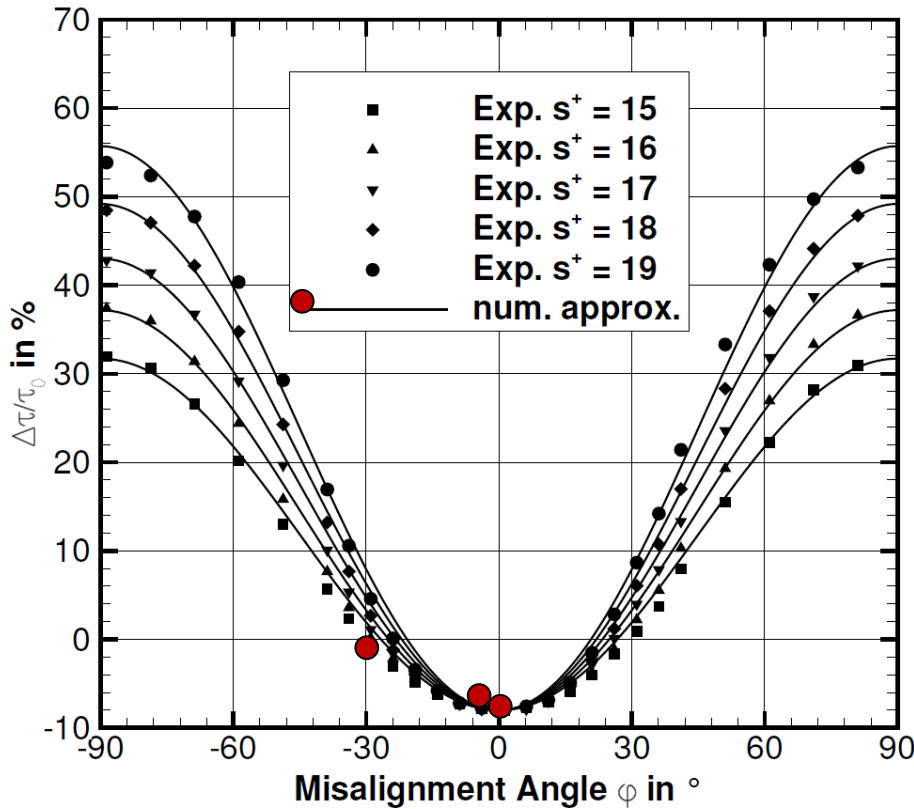
- Ideal trapezoidal riblets with $s^+ = 17$
- Riblet height $h^+ = 0.5s^+$
- Riblet tip-angle: $\alpha = 30^\circ$
- Body-fitted hexa mesh
- Variation of mean flow angle $\alpha = 0^\circ; 5^\circ; 30^\circ; 45^\circ$
- $Re_\tau = 180$ with $Re_B = 5700$
- Spatial resolution (33 million nodes):
 - $\Delta y^+ = 0.4 \dots 10$
 - $\Delta x^+ = \Delta z^+ = 1$
- Averaging for $t^+ = 25$



Integral Effect on Wall Friction

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$$\left. \frac{\Delta\tau}{\tau_{\text{smooth}}} \right|_{0^\circ} = -7.73\%$$

$$\left. \frac{\Delta\tau}{\tau_{\text{smooth}}} \right|_{5^\circ} = -6.28\%$$

$$\left. \frac{\Delta\tau}{\tau_{\text{smooth}}} \right|_{30^\circ} = -1.21\%$$

$$\left. \frac{\Delta\tau}{\tau_{\text{smooth}}} \right|_{45^\circ} = +37.47\%$$

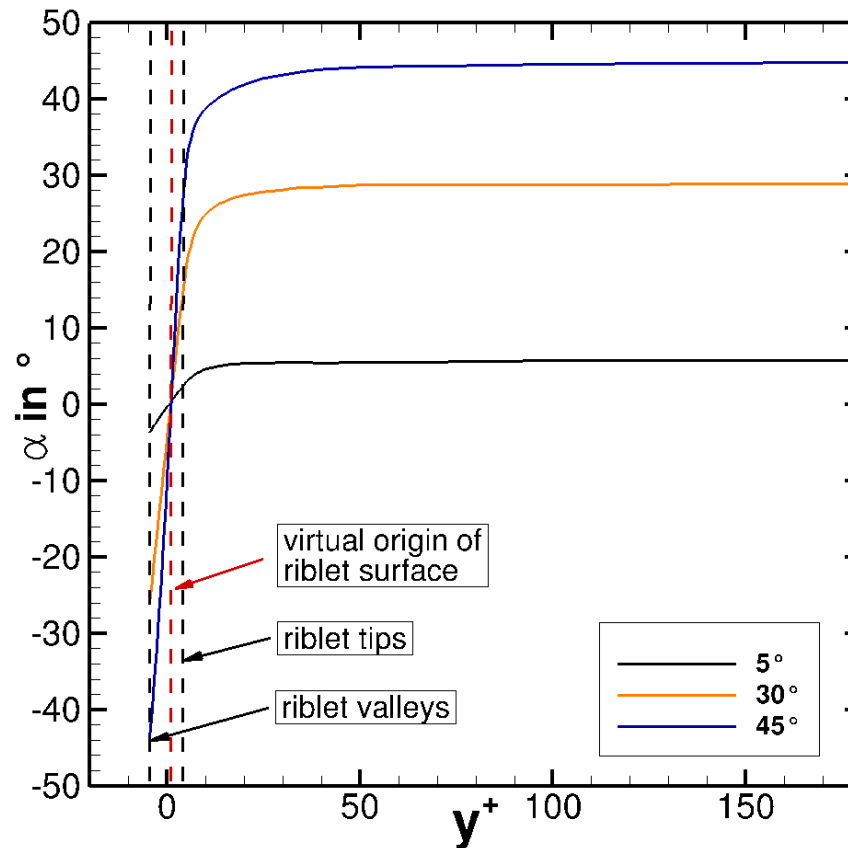
- Principal trend captured
- Slightly under-predicted for 30°
- Significantly over-predicted for 45°
- Notable coincidence with RANS predictions of compressor cascade



Mean Flow Angle α of the Wall-Parallel Components

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- Prescribed misalignment angle a attained in main flow
- Near-wall reduction of a
→ Increased shear
- Opposite flow direction in Riblet valley
- All curves intersect at one wall-normal point: $y^+ = 1.02$
→ Virtual origin of riblet surface (red dashed line)

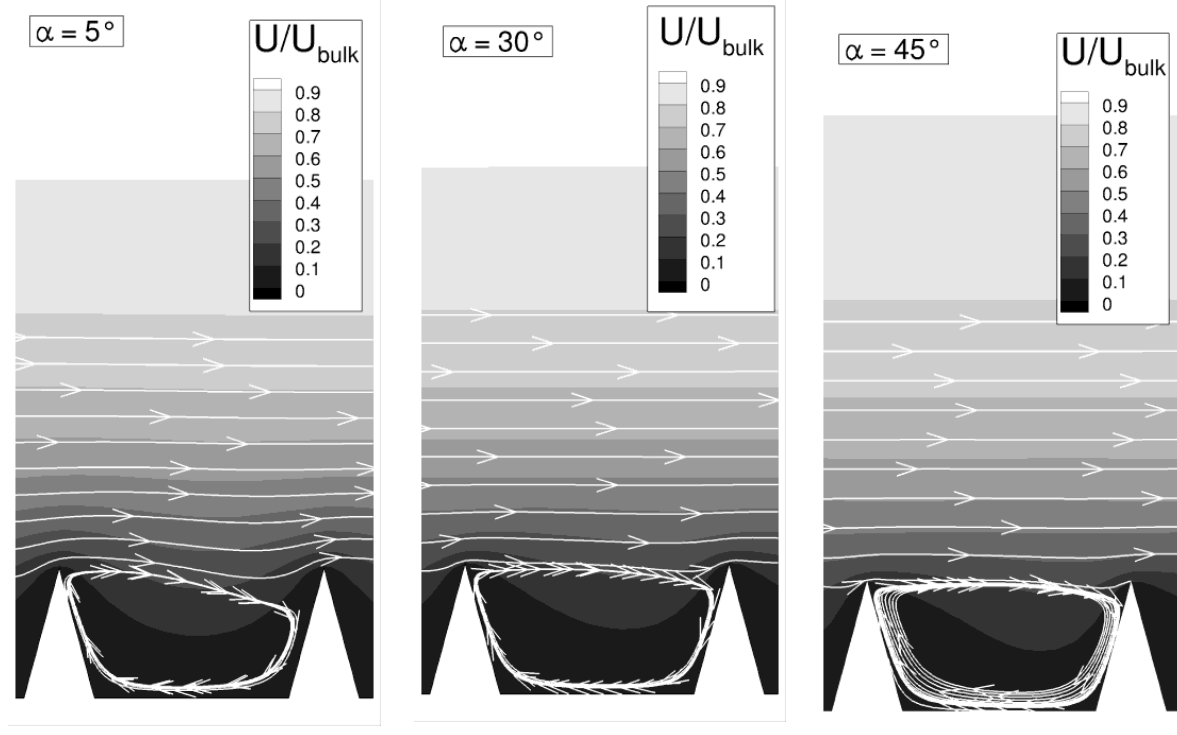


Cross-Flow Streamlines of Mean Flow

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cross-flow direction



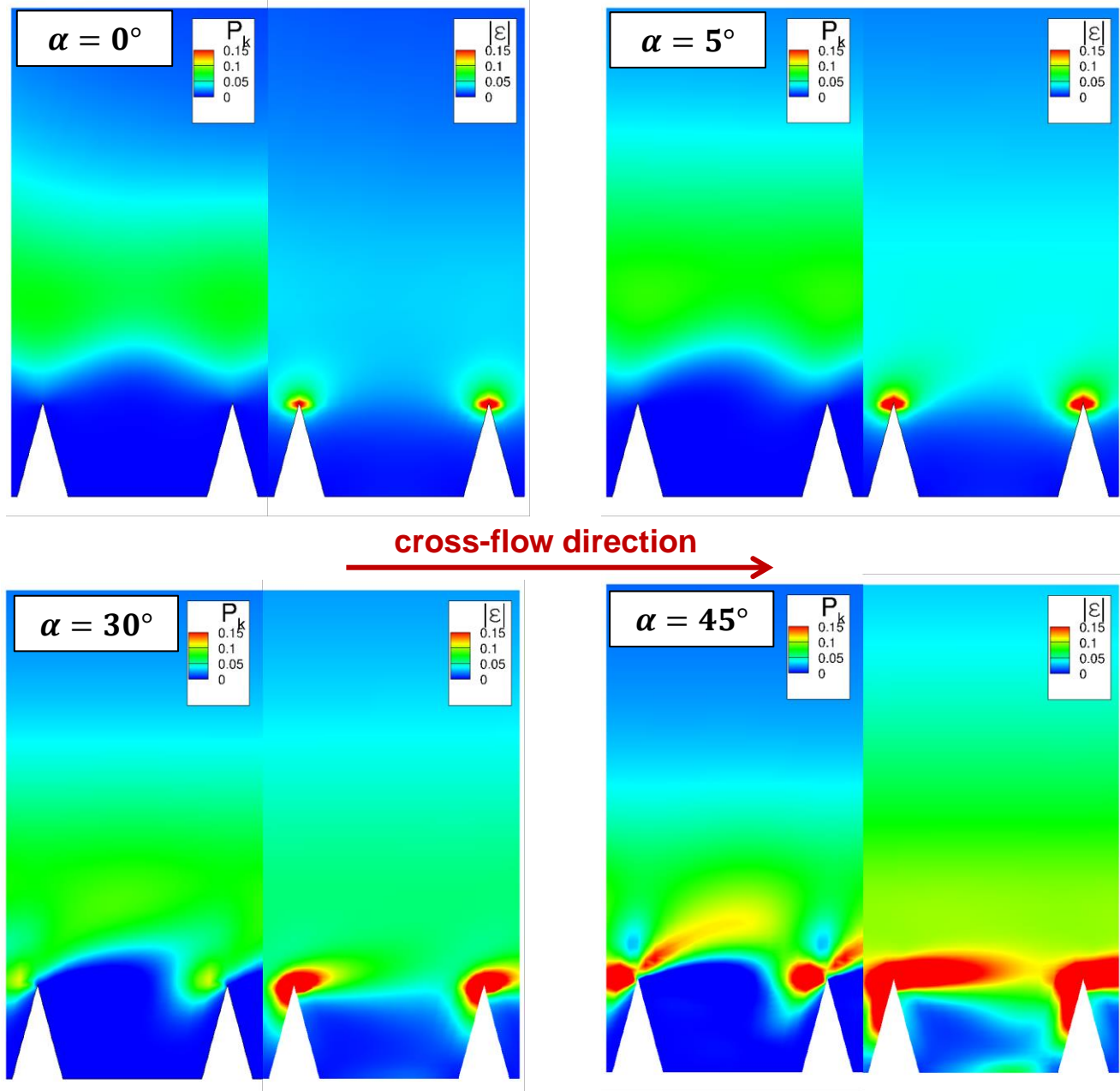
Turning of mean flow may result from vortical cross-flow in Riblet valley



Turbulent Kinetic Energy Balance

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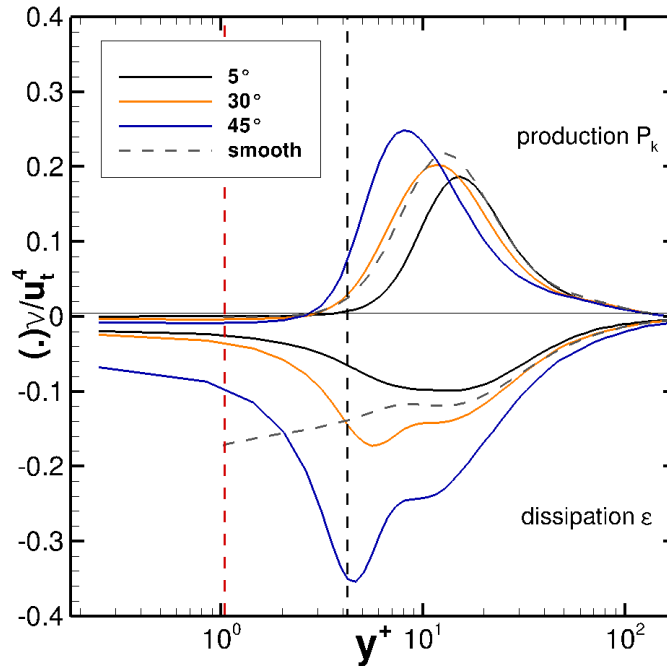


Wall-Normal Profiles at Mid-Valley

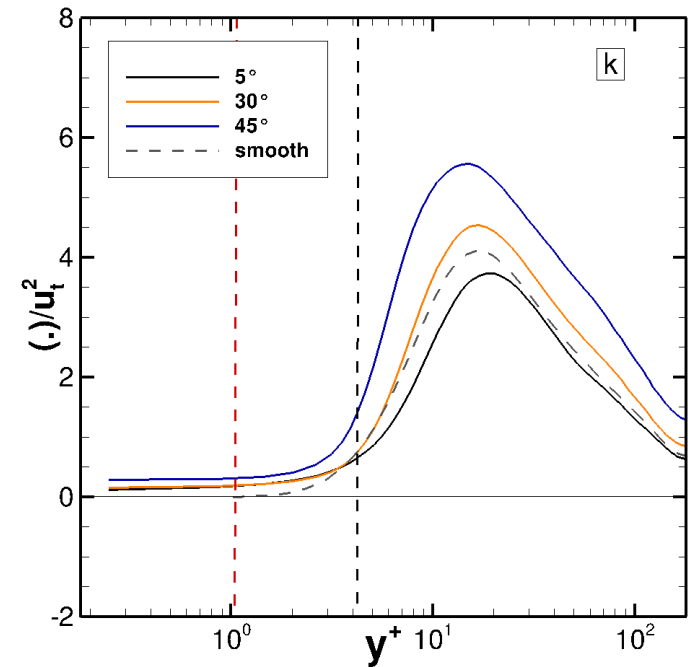
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Turbulent Kinetic Energy Balance



Turbulent Kinetic Energy



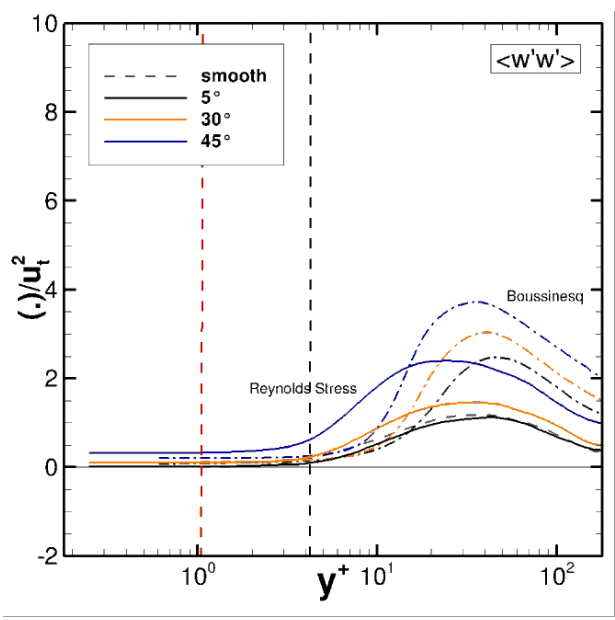
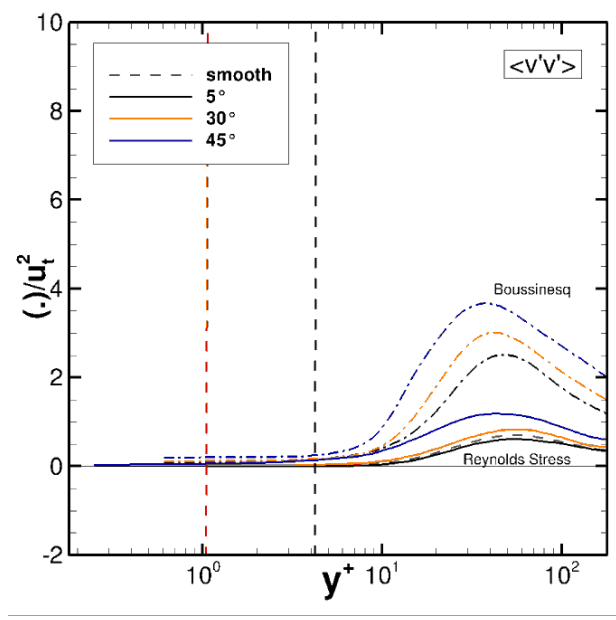
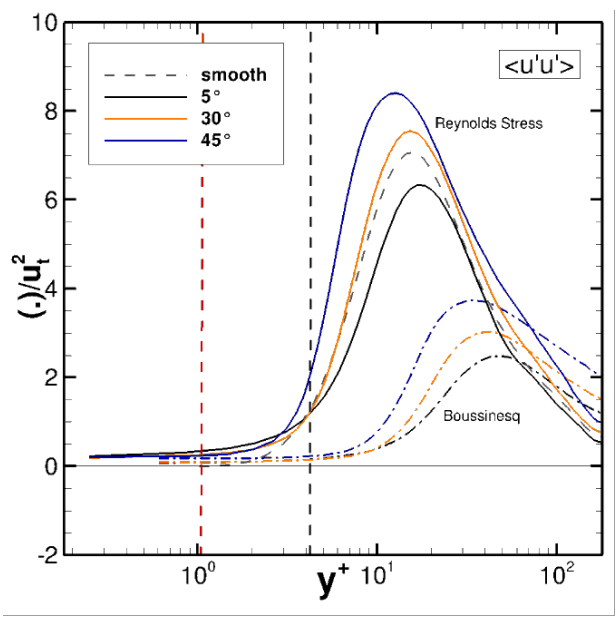
- Maxima of production and dissipation move closer to surface for increasing misalignment a
- Production P_k increases with a
→ **Effect of shear?**
- Dissipation doubles from 30° to 45°
- For drag-neutral case (30°) P_k and k nearly coincide with smooth-case...
- ...dissipation not
→ **Dissipation most sensitive quantity**



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Reynolds Normal Stresses: Resolved vs. Ideal Boussinesq



Note: wall-parallel stresses transformed acc. to α

- Resolved $\overline{w'w'}$ doubles from 30° to 45°
- Other stresses increase but relatively less
- Boussinesq captures neither basic anisotropy and its change
- nor the peak positions



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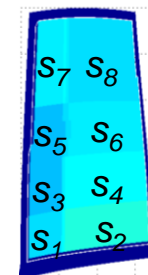
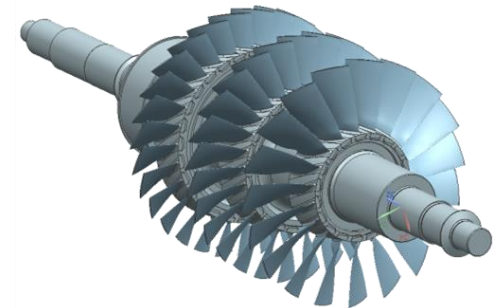
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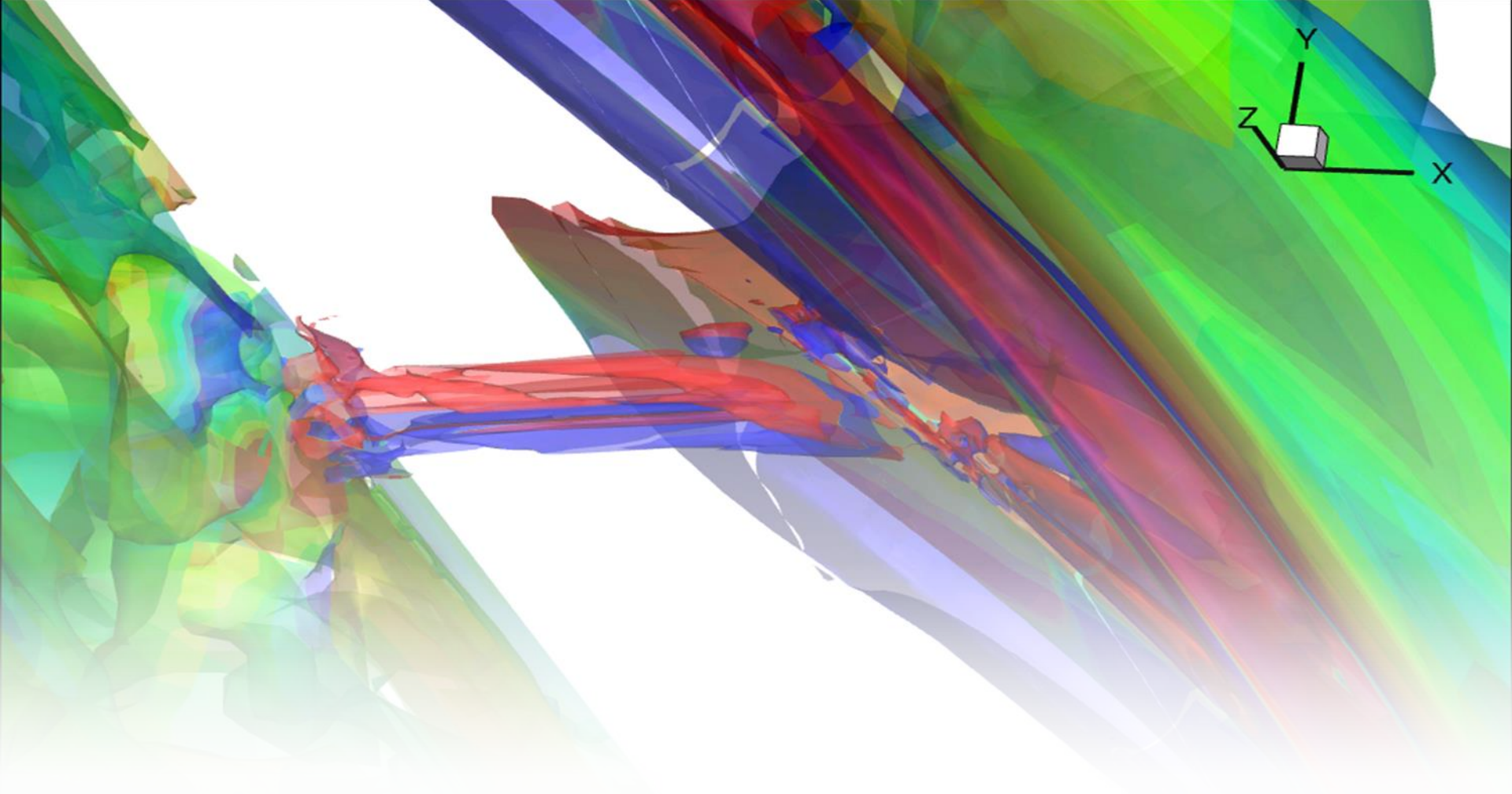
Conclusions

- DNS results successfully validated
- Misalignment effect slightly deviates from oil channel experiment but correlates with cascade experiments
- Misaligned Riblets turn the mean flow in the wall-near region due to induced cross-flow vortices in Riblet valleys
- Increasing misalignment increases maxima of turbulent quantities and shifts them closer to wall
- Turbulent kinetic energy and its production correlate with drag change
- Dissipation does not
- Ideal Boussinesq Reynolds stresses do not capture anisotropy

Outlook

- Re-assess RANS model regarding
 - turning of mean flow in wall-near region
 - relevance of anisotropy
 - empiric correlations for dissipation
- Evaluation of local loss contributions (viscous vs. turbulent stresses)
- Compressor rig validation (in preparation)



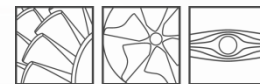


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